# Characterization of the MIC/MILC Interface and Its Effects on the Performance of MILC Thin-Film Transistors

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Abstract—Process and material characterization of the crystallization of amorphous silicon by metal-induced crystallization (MIC) and metal-induced lateral crystallization (MILC) using evaporated Ni has been performed. An activation energy of about 2 eV has been obtained for the MILC rate. The Ni content in the MILC area is about 0.02 atomic %, significantly higher than the solid solubility limit of Ni in crystalline Si at the crystallization temperature of 500 °C. A prominent Ni peak has been detected at the MILC front using scanning secondary ion mass spectrometry. The MIC/MILC interface has been determined to be highly defective, comprising a continuous grain boundary with high Ni concentration. The effects of the relative locations of this interface and the metallurgical junctions on TFT performance have been studied.

Index Terms—Grain boundary, MILC, nickel, thin-film transistor.

## I. INTRODUCTION

ETAL induced crystallization (MIC) of amorphous silicon (a-Si) using nickel (Ni) has been achieved at a temperature ( $\sim$ 500 °C) [1]–[3] much lower than that ( $\sim$ 600 °C) typically used for solid phase crystallization (SPC) without Ni. However, the significant incorporation of Ni in the MIC polycrystalline silicon (poly-Si) films [4] might limit the potential improvement in the performance of the thin film transistors (TFT's) realized on such films. Subsequently, metal induced lateral crystallization (MILC) has been proposed [5] as a better alternative to MIC, resulting in poly-Si films with reduced Ni incorporation and large elongated grains—the long axes of which are parallel to the direction of the grain

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growth [4]. Low temperature TFT's with high field effect mobility have been fabricated [6]–[8], thus establishing MILC as a potentially enabling technology for realizing systems requiring low process temperature yet with high performance transistors—such as the active matrix liquid crystal displays with on-panel integrated driver circuits.

While no measurable amount of Ni has been detected within the MILC region using either transmission electron microscopy (TEM) [5], [6] or Auger electron spectroscopy (AES) [4], none of these techniques are particularly appropriate for trace element detection. Therefore, it is still not clear how Ni is distributed, from inside the MIC region, across the MIC/MILC interface, through the MILC region and finally across the MILC front to inside the a-Si region. This crucial but missing information might be particularly relevant to the unexpectedly high leakage current measured in conventional MILC TFT's [9], in which the edge of the MIC region is self-aligned to the edge of the transistor channel region. Furthermore, while the crystal grains are indeed larger in MILC poly-Si films [4], [6], the corresponding field effect mobility is still lower than those typically reported for poly-Si films obtained using laser crystallization [10] or SPC of Si implanted a-Si [11]. This suggests that the crystal grains in low temperature MILC films may be less ideal and may contain a significant number of intra-granular defects.

In this work, scanning secondary ion mass spectrometry (SIMS) and energy dispersive X-ray microanalysis (EDX) have been used to detect the distribution of Ni in laterally crystallized a-Si films. SIMS was performed on a Cameca IMS-4F platform, while TEM and EDX were performed on a Philips CM20 transmission electron microscope equipped with an Oxford Instruments ISIS EDX system. High resolution TEM has been used for crystallite defect characterization. The effects of the MIC/MILC interface on device performance have been characterized by constructing TFT's with the interface either self-aligned to or offset from the metallurgical junctions.

#### II. MATERIAL CHARACTERIZATION

For the material analyses, 100 nm thick a-Si films were deposited by the pyrolysis of SiH<sub>4</sub> at 550 °C in a low-pressure chemical vapor deposition (LPCVD) reactor. The starting substrates were either oxidized (100)-oriented silicon wafers or Corning 7059 glass coated with 500-nm thick low temperature (425 °C) LPCVD oxide (LTO). Approximately 5 nm of Ni was deposited by electron-beam evaporation on selected



Fig. 1. Dependence of the MILC rate on the reciprocal of "kT," where "k" is the Boltzmann constant in eV/K and "T" is the heat treatment temperature in K.

a-Si regions using a photoresist masked lift-off process. The substrate temperature was maintained below 100 °C during the evaporation. Crystallization was carried out in a conventional atmospheric pressure furnace at temperature varying from 425–550 °C. The ambient during the heat treatment was high purity N<sub>2</sub> gas evaporated from a liquid source. The resulting MILC length was measured using an optical microscope.

The MILC rate, estimated by dividing the total MILC length by the total heat treatment time, is plotted in Fig. 1 as a function of the reciprocal of the product of the absolute crystallization temperature and the Boltzmann constant. For a given temperature, a slightly lower MILC rate has been obtained on LTO coated glass than on oxidized silicon, with activation energy  $(E_a)$  of 1.97 and 2.06 eV, respectively. These values are significantly larger than the 1.5 eV obtained for the crystallization of cosputtered a-Si(0.5% Ni) [12]. This implies the mechanism of MILC, even if not entirely different from that of the crystallization of cosputtered a-Si(0.5% Ni), may at least involve a different rate limiting step.

Ni distribution in the MIC, the MILC and the a-Si regions has been obtained using scanning SIMS. The entire area of the sample was divided into 256 sampling points. A 1  $\mu$ m diameter beam of oxygen ions at 15 keV was scanned sequentially from one point to the next, with each point sputtered for about 0.9 s. A total of 500 passes were made over the collection of points, thus sputtering through the entire depth of the film at each sampling point. A two-dimensional (2-D) distribution of the integrated secondary Ni ion yield, expressed as brightness intensity, is plotted in Fig. 2. As expected, the MIC region is the brightest, indicating the highest Ni concentration. However, while no Ni was detected in the MILC region using the less sensitive AES [4], low levels of Ni, as indicated by the scattered bright spots, have been detected using SIMS. Interestingly, a dense population of bright spots also has been detected along the interface of the a-Si and the MILC regions, thus conclusively proving that the MILC front is rich in Ni. The secondary Ni ion count across a line-scan is shown in Fig. 3(a). It should be noted that the shape of this lateral Ni distribution is almost identical to that in the



Fig. 2. Two-dimensional distribution of Ni obtained by scanning micro-SIMS analysis of the MIC, the MILC, and the a-Si regions. The Ni concentration is proportional to the brightness and the density of the spots. A high concentration of Ni, about 0.4 atom %, is observed at the MILC front.

vertical direction [4], obtained using X-ray photo-electron spectroscopy in the MIC region. This strongly supports the proposition [4] that the MILC front is populated by a high concentration of Ni containing nodules, which are ultimately responsible for the low temperature crystallization.

The results of an EDX scan (5-nm spot size) across the MILC front are presented in Fig. 3(b). Since the signal near the front, though erratic, is clearly above the noise level measured in both the a-Si and the MILC silicon regions, it can be used to roughly estimate the corresponding Ni concentration. A value of 0.4 atomic % has been obtained. This value can be used to calibrate the peak of the secondary Ni ion count at the MILC front shown in Fig. 3(a). Furthermore, if it is assumed that this calibration is also valid inside the MILC region, a rough estimate of about 0.02 atomic % can be obtained for the corresponding Ni concentration. This finite concentration of Ni in the MILC region is again consistent with the proposition that slower moving Ni containing nodules would be trapped [4] in the grain boundaries in the MILC region.

A width of about 0.5  $\mu$ m can be estimated from the EDX scan for the Ni rich MILC front in Fig. 3(b). The total amount of Ni within this front is roughly equal to the product of its width and the corresponding Ni concentration of 0.4 atomic %. This is just enough to supply the steady state Ni concentration of 0.02 atomic % in about 10  $\mu$ m of the MILC length. Clearly, a constant supply of Ni is needed to sustain the Ni concentration at the MILC front during crystallization. This supports the proposition [13] that a continuous flux of Ni, flowing from the MILC region to the MILC front, exists inside the MILC region during steady state MILC.

A TEM micrograph showing a rugged crystallization front is presented in Fig. 4. One can observe isolated crystallized re-



Fig. 3. Distribution of Ni across: (a) the MIC, the MILC, and the a-Si regions obtained by SIMS and (b) across the MILC front obtained by EDX.

gions, terminated by darker specs of material, protruding from the MILC region and surrounded on three sides by a-Si. The spec of material is most likely the Ni containing  $NiSi_x$  nodule moving at the crystallization front and responsible for the corresponding Ni peak detected by SIMS.

A higher magnification TEM micro-graph of the MILC region is shown in Fig. 5(a). Clearly the grains are highly defective, which explains the streaks around the predominantly {110} electron diffraction pattern shown in Fig. 5(b). Some of these defects are more visible in the high resolution TEM micrograph shown in Fig. 5(c), indicating the existence of line defects and stress field induced brightness contrast. Therefore the MILC grains, while large, nevertheless contain a large number of intragranular defects. This could be the reason [14] that smaller field effect mobility has been measured on MILC-TFT's than on poly-Si TFT's fabricated on laser crystallized a-Si [10], [14] or solid phase crystallized Si implanted a-Si [11].



Fig. 4. TEM micrograph of a rugged MILC front. Protrusions of crystallized silicon inside the a-Si are terminated by specs of material with darker contrast.

In addition to the high Ni concentration near the MIC/MILC interface [Fig. 3(a)], a fuzzy but continuous grain boundary also coincides with this interface, as shown in the TEM micrograph in Fig. 6. It can be anticipated that such a "defective" MIC/MILC grain boundary (MMGB) would have significant electrical effects [14], [16], if placed inside the high electric field region of a reverse biased junction.

## **III. DISCUSSION**

The  $E_a$  value of 1.97 or 2.06 eV for the MILC rate is much larger than that of the diffusion constant of Ni either in crystalline Si (0.76 eV) [17] or in a-Si (1.3 eV) [18]. Given the proposition that MILC is an "interfacial" process mediated by Ni diffusion across  $NiSi_x$  nodules at the crystallization front [4], [19], it is not surprising that neither Ni diffusion across the MILC region nor its diffusion into the a-Si region are the rate controlling steps in MILC. Interestingly, the MILC  $E_a$  values extracted from the two different kinds of substrates, while significantly different from the 1.55 eV for NiSi formation and the 2.9 eV for NiSi degradation [20], are much closer to the value of 2.08 eV for Ni induced lateral secondary grain growth in poly-Si reported by Hong et al. [20] and the 1.9 eV for Au induced poly-Si recrystallization reported by Allen et al. [21]—who suggested that the activation energy could be attributed to the energy required to attach a Si atom to the growing crystallization front.

The 0.02 atomic % Ni estimated inside the MILC region is significantly larger than the solid solubility of no more than  $10^{16}$ /cm<sup>3</sup> for Ni in crystalline silicon at 500°C [16]. Consequently, the most likely source of the secondary Ni ions detected by SIMS in the MILC region is the Ni containing nodules



Streaks

(b)



(c)



Fig. 6. TEM micrograph showing a distinct grain boundary separating the MIC and the MILC regions.

trapped in the grain boundaries [4], rather than the continuous flux of dissolved Ni in the MILC region.

#### **IV. DEVICE FABRICATION**

For studying the impact of the MIC/MILC interface on TFT performance, devices were fabricated on 100 mm silicon wafers covered with 100 nm thick thermal oxide. A thin 100 nm LPCVD a-Si layer was first deposited at respective pressure and temperature of 300 mtorr and 550 °C. After patterning the a-Si layer to form the active islands, a 100-nm thick layer of LTO gate insulator and 200-nm thick a-Si gate electrode were deposited. The wafers were thoroughly cleaned after the gate electrode patterning and the exposure of selected areas in the source and drain regions. About 2 nm of Ni was deposited in an ultra-high vacuum evaporation system. Subsequently, the source, drain, and gate regions were doped by self-aligned phosphorus implantation at a dose of  $3 \times 10^{15}$ /cm<sup>2</sup> and an energy of 40 keV. The wafers were then heat-treated at 500 °C, during which simultaneous Ni induced crystallization of the a-Si layers and dopant activation were accomplished. Finally, contact holes were opened through 500 nm of LTO insulation layer, Al-1% Si was sputter deposited and the devices were sintered in forming gas at 400 °C for 30 min. For some of the devices, hydrogen plasma passivation was performed in a 13.56 MHz parallel plate reactor at 300 °C in a 300 mtorr gas mixture of 200 sccm H<sub>2</sub> and 100 sccm N<sub>2</sub>.

# V. DEVICE CHARACTERIZATION

Fig. 5. Crystal quality analyses with: (a) TEM micrograph showing a high density of defects, (b) TED micrograph showing a (110) diffraction pattern. (the presence of the streaks indicates imperfections in the material), and (c) high resolution TEM micrograph showing line defects and stress field induced brightness contrast.

Schematic cross-sections of MILC TFT's with three different MMGB locations relative to the source and drain junctions, together with the device models at low drain voltage  $(V_d)$  and



Fig. 7. Schematic cross-sections, device models at low  $V_d$  and the associated potential barriers across the channels of (a) a conventional MILC TFT with the MMGB's self-aligned to both source and drain junctions,(b) an MILC TFT with a one-sided offset, and (c) an MILC TFT with double-sided offsets.

the potential distribution across the channels, are shown in Fig. 7. Device characterization was performed at room temperature using an HP4156 Precision Semiconductor Parameter Analyzer.

Shown in Fig. 8 is the dependence of the low  $V_d$  (0.1 V) drain current ( $I_d$ ) on the gate voltage ( $V_g$ ) of a) a conventional MILC TFT, b) a MILC TFT with the MMGB offset from the drainjunction, and c) a MILC TFT with the MMGB's offset from both source and the drain junctions. No hydrogenation has been performed on the devices for this set of measurements. Clearly, the overall  $I_d-V_g$  characteristics and the apparent threshold voltage ( $V_t$ ) of the first two devices are almost identical, where  $V_t$  is defined as the  $V_g$  needed to achieve an  $I_d = W/L \times 10$  nA. W and L are the width and length of the TFT, respectively. On the other hand, the  $V_t$  value of the device with the double-sided offset is comparatively smaller.



Fig. 8.  $I_d - V_g$  characteristics of the three different kinds of MILC TFT's.



Fig. 9. Effects of plasma hydrogenation on the  $I_{d}-V_{g}$  characteristics of conventional MILC TFT's, with the MMGB's self-aligned to the metallurgical junctions.

When an MMGB coincides with any one of the metallurgical junctions, it becomes part of the channel. The high density of grain boundary trap states effectively raises the local, hence also the overall,  $V_t$  and the subthreshold slope (S) of the device. Only by removing the MMGB's from both junctions can one effectively reduce  $V_t$  and S. However, it should be noted that the difference in this  $V_t$  is only apparent and does not lead to an increase in  $I_d$  at sufficiently high  $V_g$  [22] This is because an MMGB, being a grain boundary, has a very small lateral extent. Consequently, it can be considered as a TFT with a very short channel length, albeit with a higher  $V_t$ . While conduction at low  $V_g$  is limited by such high  $V_t$  MMGB TFT [Fig. 7(a)], it is limited at high  $V_g$  by the resistance of the intrinsic MILC "long" channel TFT [Fig. 7(c)], which is common to all three device structures regardless of the locations of the MMGB's.

Clearly, the effect of the localized high- $V_t$  MMGB TFT becomes more prominent as the channel length is reduced. This is responsible for the reverse short channel effect [23] recently



Fig. 10. Dependence of the drain current on the gate voltage. The off-state leakage current of the testing configurations with the MMGB self-aligned or offset from the drain metallurgical junctions are compared.



Fig. 11. Dependence of the drain current on the drain voltage at different gate voltage. Kink effects of the testing configurations with the MMGB self-aligned to or offset from the drain metallurgical junctions are compared.

reported for MILC TFT's with overlapping MMGB's and metallurgical junctions.

Since the high apparent  $V_t$  is caused by the high density of MMGB traps, it should also be possible to reduce this  $V_t$  by passivating the traps. This is demonstrated in Fig. 9. Unlike the data shown in Fig. 8, those in Fig. 9 show an increase in  $I_d$  at high  $V_g$ . This is because the MILC channel, in addition to the MMGB's, was also partially passivated by the hydrogen plasma [24].

The dependence of the  $I_d$  on  $V_g$  at high  $V_d$  (10.1 V) is shown in Fig. 10. The off-state ( $V_g < 0$  V) leakage current ( $I_{lk}$ ) for the testing configuration with the MMGB off-set from the drain junction is significantly lower than that for the configuration with the MMGB self-aligned to the drain junction. Since  $I_{lk}$ at high  $V_d$  is dominated by trap-assisted field-emission current, the combination of high electric field in the junction and high trap density in the overlapping MMGB will result in significantly higher  $I_{lk}$ , when compared to the case with the defective MMGB offset from the drain junction and located deep inside the quasineutral drain region [9].

Substrate current resulting from impact ionization at a sufficiently large  $V_d$  is known to lower the threshold voltage via a modulated body potential. This is manifested as current kinks in the  $I_d-V_d$  (Fig. 11) curves of the testing configuration with the MMGB self-aligned to the drain junction [25]. When the source and drain terminals are interchanged so that the MMGB is offset from the drain junction, the current kinks are suppressed. This shows that when the MMGB overlaps the drain junction, either the drain electric field or the impact ionization rate is enhanced due to the presence of charged defect states, such as the grain boundary traps or the Ni containing impurities, in the MMGB.

## VI. SUMMARY

Activation energy of 1.97 and 2.06 eV for the MILC rate has been measured on the oxidized Si and on LTO coated Corning 7059 glass substrates, respectively. A high Ni concentration has been detected at the MILC front, indicating the presence of a significant amount of Ni containing species. While the concentration of Ni inside the MILC is low, it is not negligible. The MIC/MILC interface is found to be highly defective, containing both a continuous grain boundary (MMGB) and a high concentration of Ni. The overlap of the MMGB and the drain metallurgical junction is found to have detrimental effects on the apparent threshold voltage, the leakage current and the kink-effect characteristics of MILC-TFT's. Such effects can be reduced or eliminated by separating the MMGB from the junction or by hydrogen passivation.

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